

# Engineering News-Record

ALTEC

ALTEC

A QUALITY COMPANY OF LING ALTEC, INC.

1515 S. Manchester Avenue, Anaheim, California

TECHNICAL LETTER NO. 201-A

## USEFUL DIRECTIVITY DATA FOR REVERBERANT SOUND FIELDS

By

Bob Beavers, Chief Engineer, Acoustics

### CALCULATION OF DIRECTIVITY FACTOR

The directivity factor ( $Q$ ) of a loudspeaker is the ratio of the total power radiated by a hypothetical loudspeaker, having a uniform radiation pattern, to the given loudspeaker when each have identical symmetry on the principle axis of symmetry. Although the analytical calculation can be made for many simple models (1), most real loudspeakers deviate from mathematical models so that data must be taken for accurate results.

When the sound radiation pattern under examination can be considered to have radial symmetry about its principal axis; i.e., a figure of revolution; the  $Q$  can be calculated from the following integral in Equation 1.

(Eq. 1)

$$Q = \frac{2}{\int_0^{\pi/2} [P(\theta)]^2 \sin \theta d\theta}$$

Where  $Q$  is the directivity factor

$P_0$  is 1

$\theta$  is the polar angle

The graphical evaluation of this integral suggested by Bauer (2), has been used in reducing several hundred polar response curves to  $Q$ s, which are presented in the data sheets.

### TEST SETUP

Polar response patterns were run on the various horns and low-frequency loudspeakers with the test setup shown in Figure 1. One third-octave band filtered pink noise was used as a test signal, except in the broadband measurements where a 500 Hz

to 3000 Hz passband was obtained by using an ALTEC 9067B adjustable bandpass filter.

### DATA PRESENTATION

Polar patterns were obtained in both horizontal and vertical orientations wherever possible. The integral (1) was obtained by graphical means from each polar plot and the resulting  $Q$  was plotted, as a function of frequency, for each loudspeaker. This was done for both horizontal and vertical polar data. This technique offers the important advantage of providing both integrated horizontal and vertical directivity information, as well as allowing a mean  $Q^*$  figure to be calculated for the effective  $Q$  in a highly reverberant space. The mean  $Q$  figure used is a geometric mean based on the area of the rectangle formed by the horizontal and vertical coverage angles as expressed in Equation 2.

(Eq. 2)

$$\text{Mean } Q^* = \frac{\pi}{4} \sqrt{Q_H \cdot Q_V}$$

Where Mean  $Q$  is the mean directivity factor

$Q_H$  is the apparent horizontal directivity factor

$Q_V$  is the apparent vertical directivity factor

It is interesting to reverse this process and assign coverage angles to the loudspeakers, based on the concept that the total sound power radiated is through a rectangular window. These angles are indicated on the right margin of the "Q versus Frequency" curves and should be used to read a rough horizontal and vertical coverage from the  $Q_H$  and  $Q_V$  curves, respectively.

In addition to the "Q versus Frequency" curves, typical polar response patterns have been included for preferred horn-driver combinations at a 1/3-octave frequency band centered at 1000 Hz. These curves have been split in half to display both the horizontal and vertical polar response on one sheet. These curves are typical of several hundred that were recorded and that are on file for reference.

- (1) Hopkins and Stryker, Procedures of I.E.E., March, 1948, P4.
- (2) B.B. Baumzeiger (Bauer), J.A.S.A. No. 11, 1940, P477

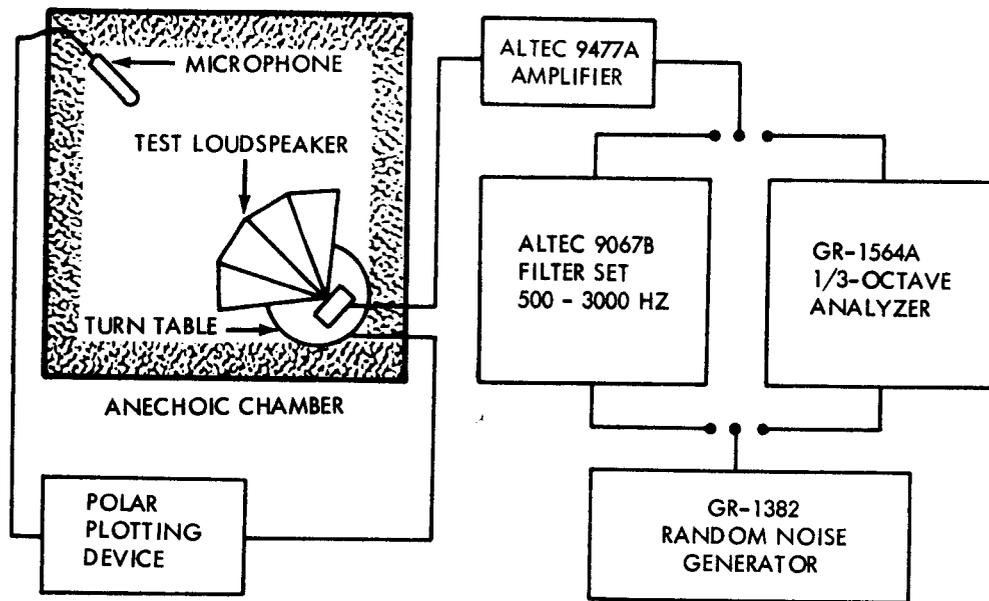
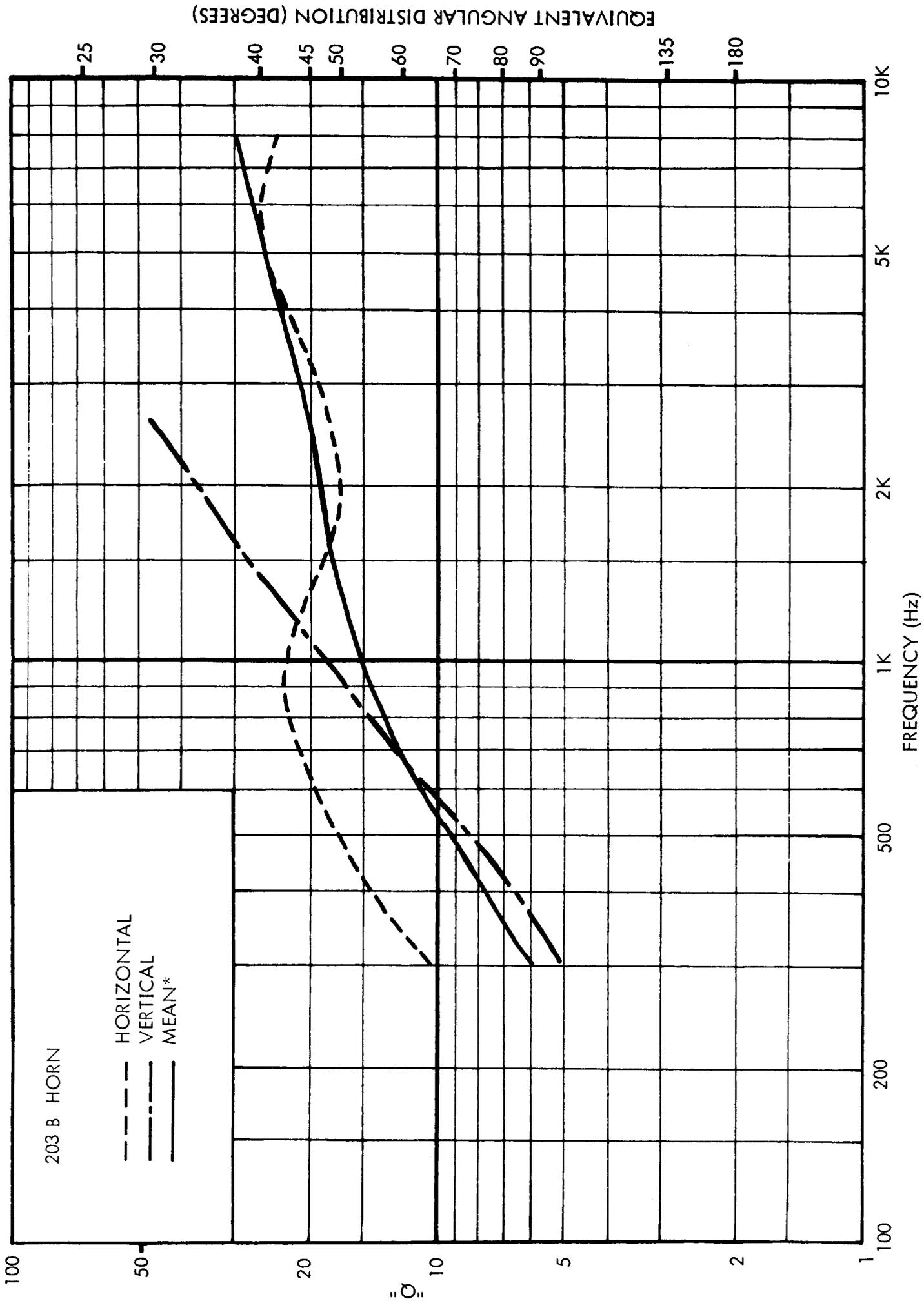
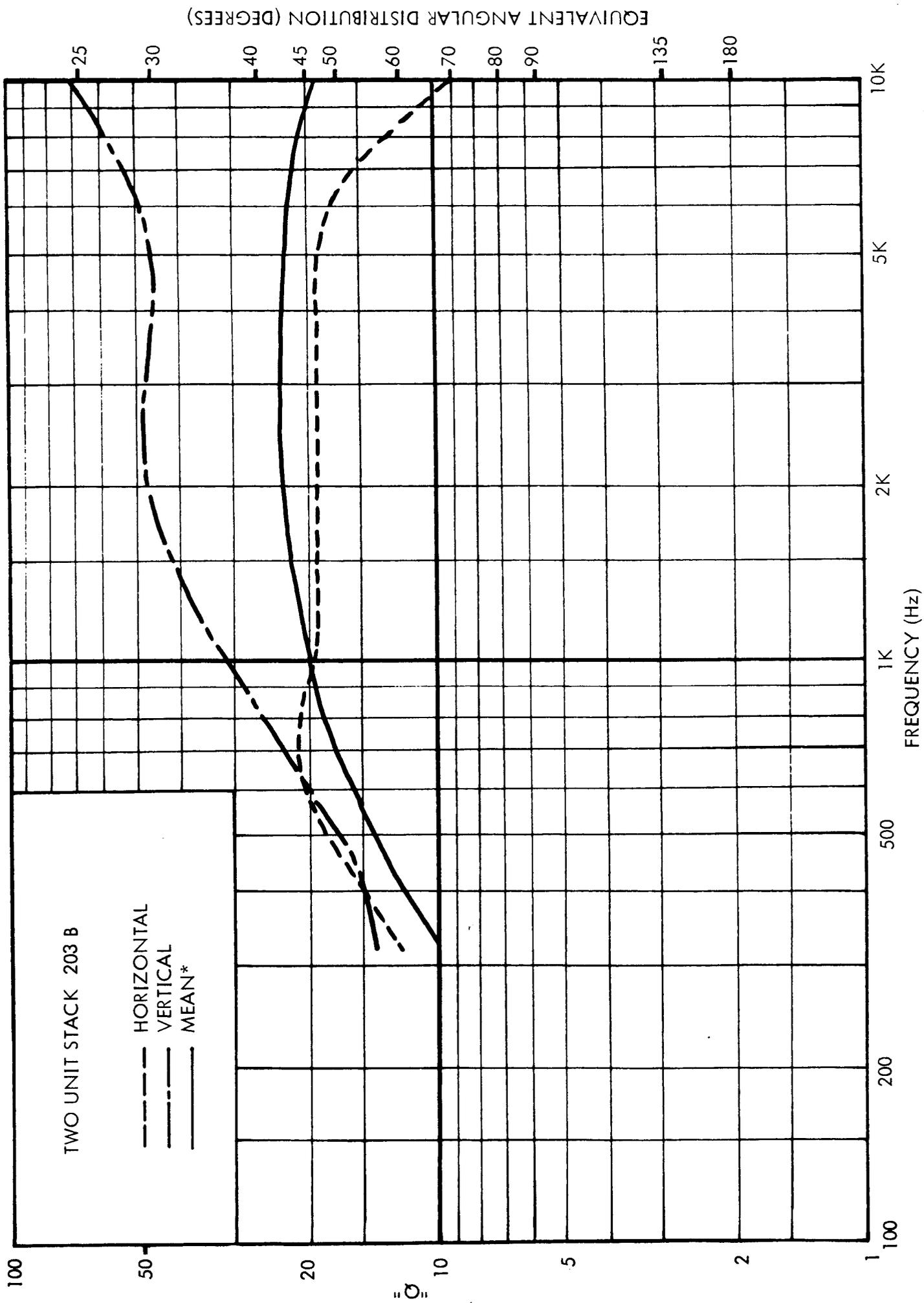


Figure 1. Test Setup for Measuring Polar Response Patterns

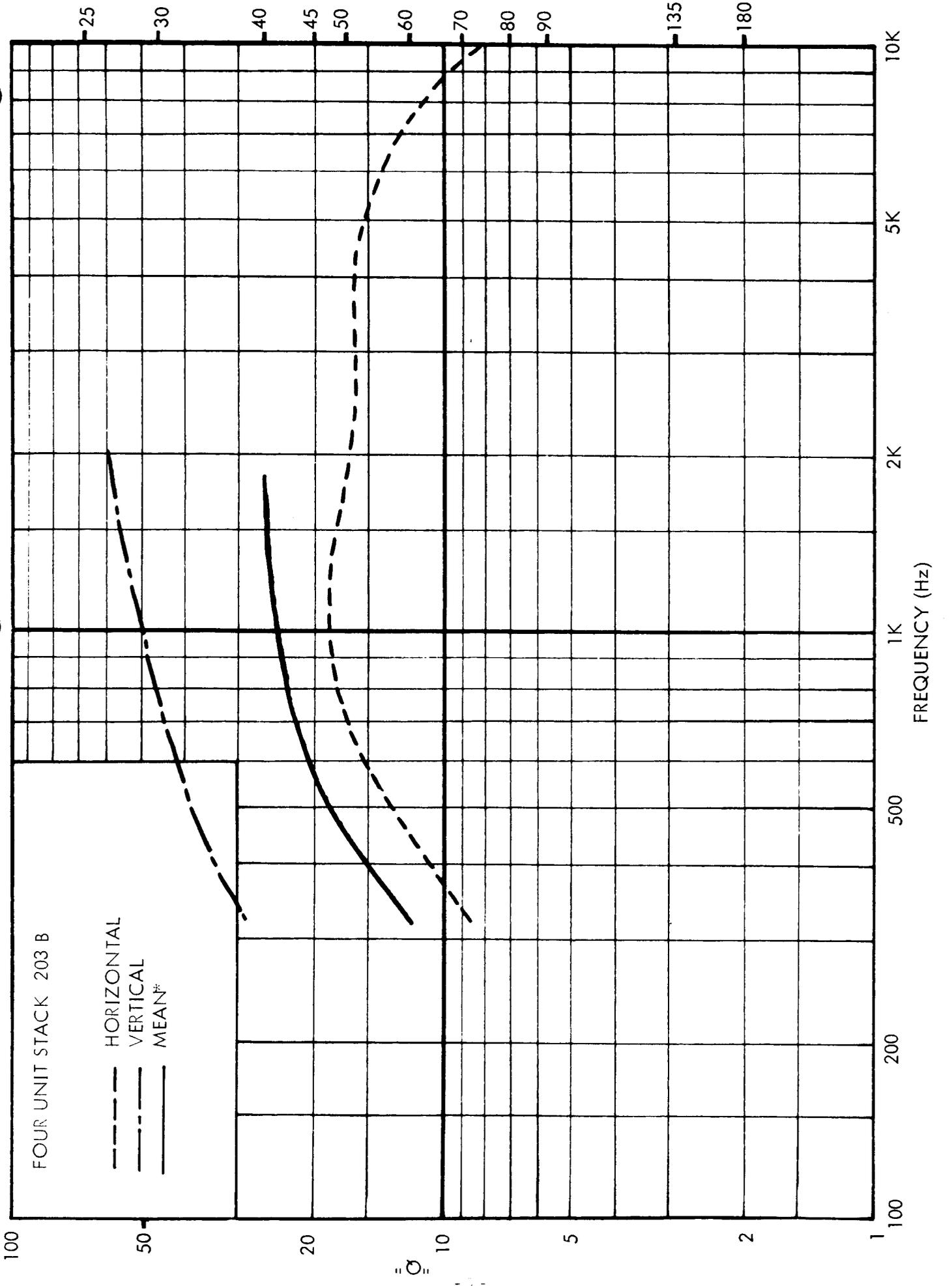


EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

FREQUENCY (Hz)



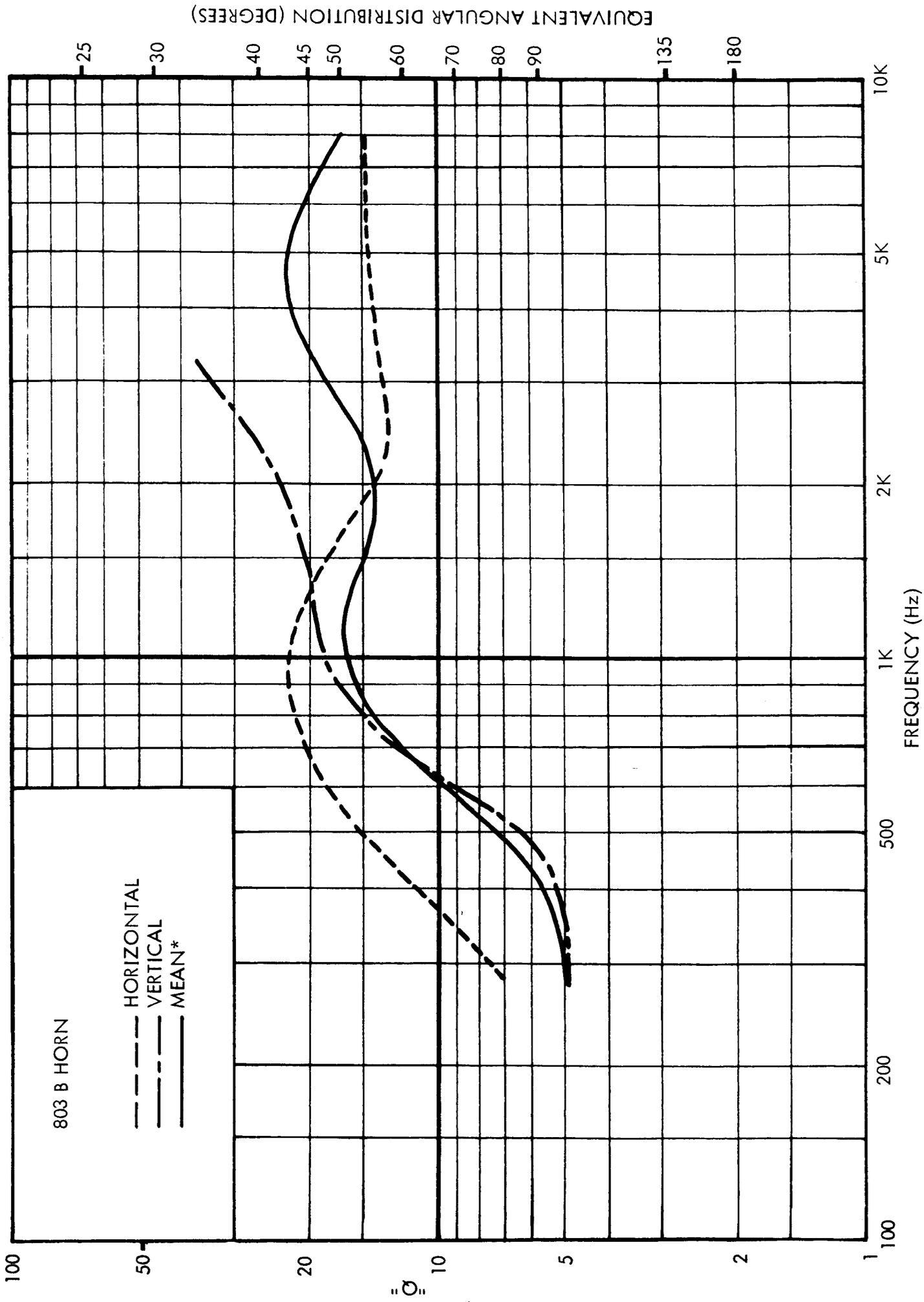
EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)



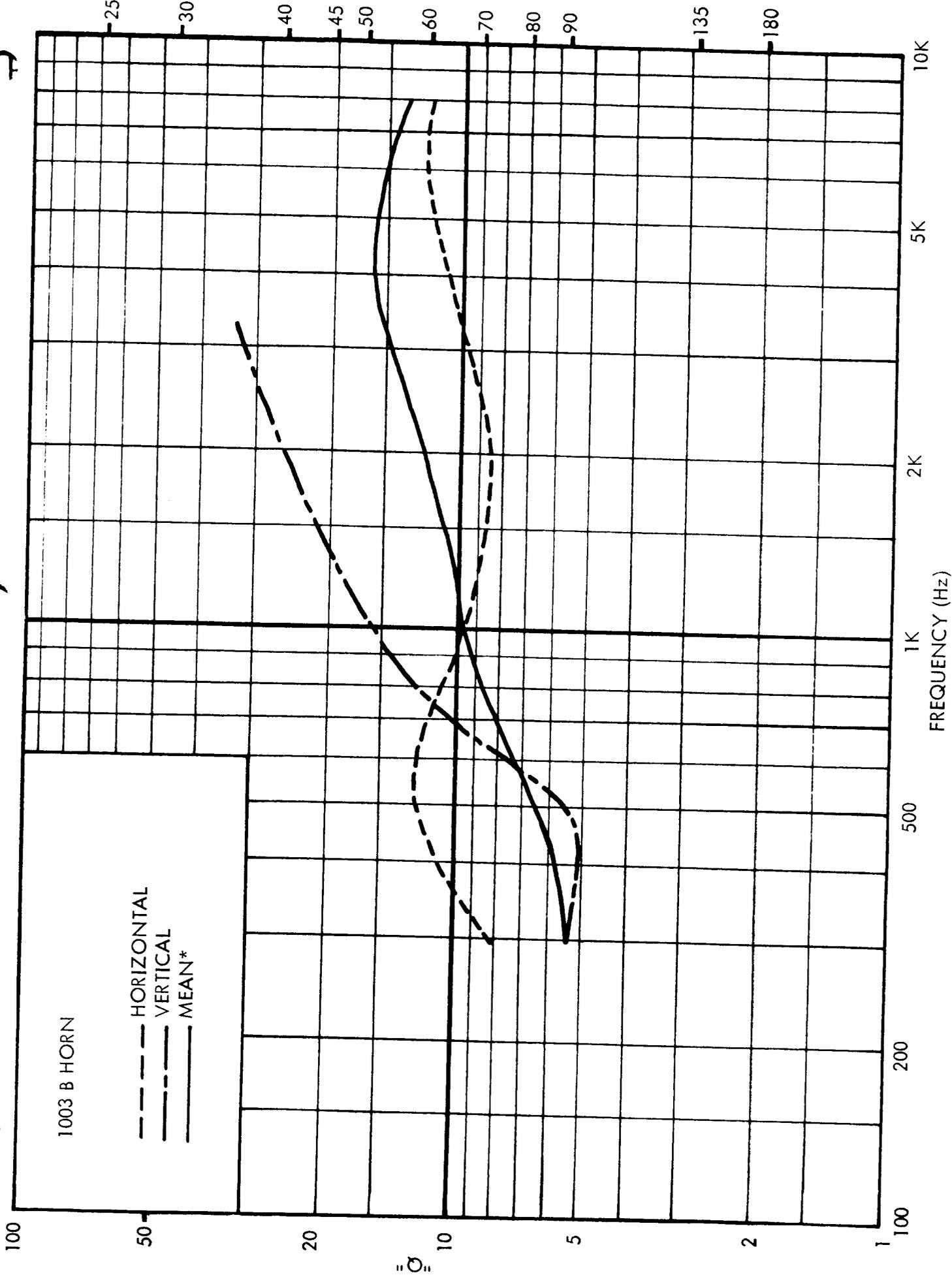
FOUR UNIT STACK 203 B

FREQUENCY (Hz)

$\theta$



EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)



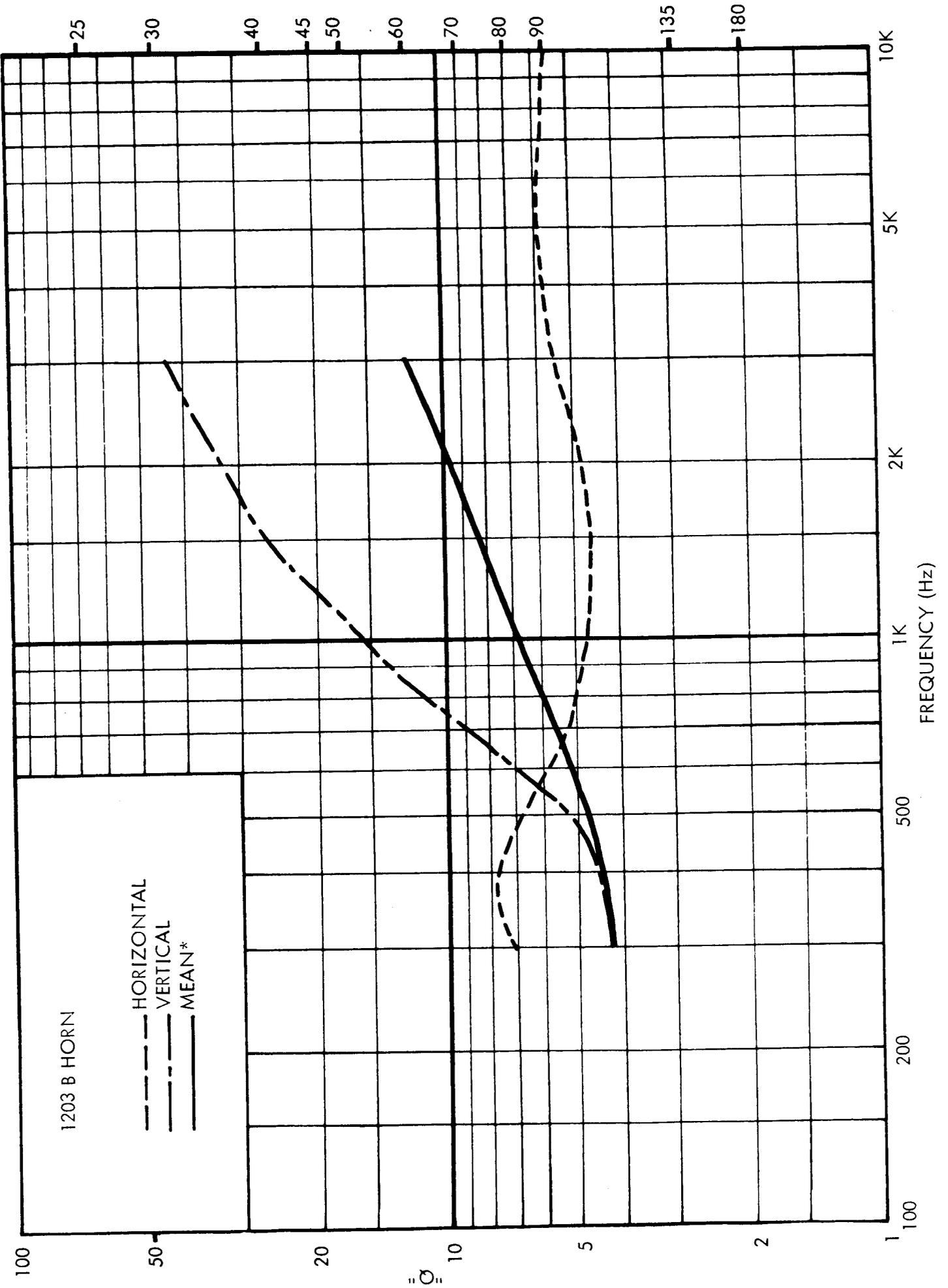
1003 B HORN

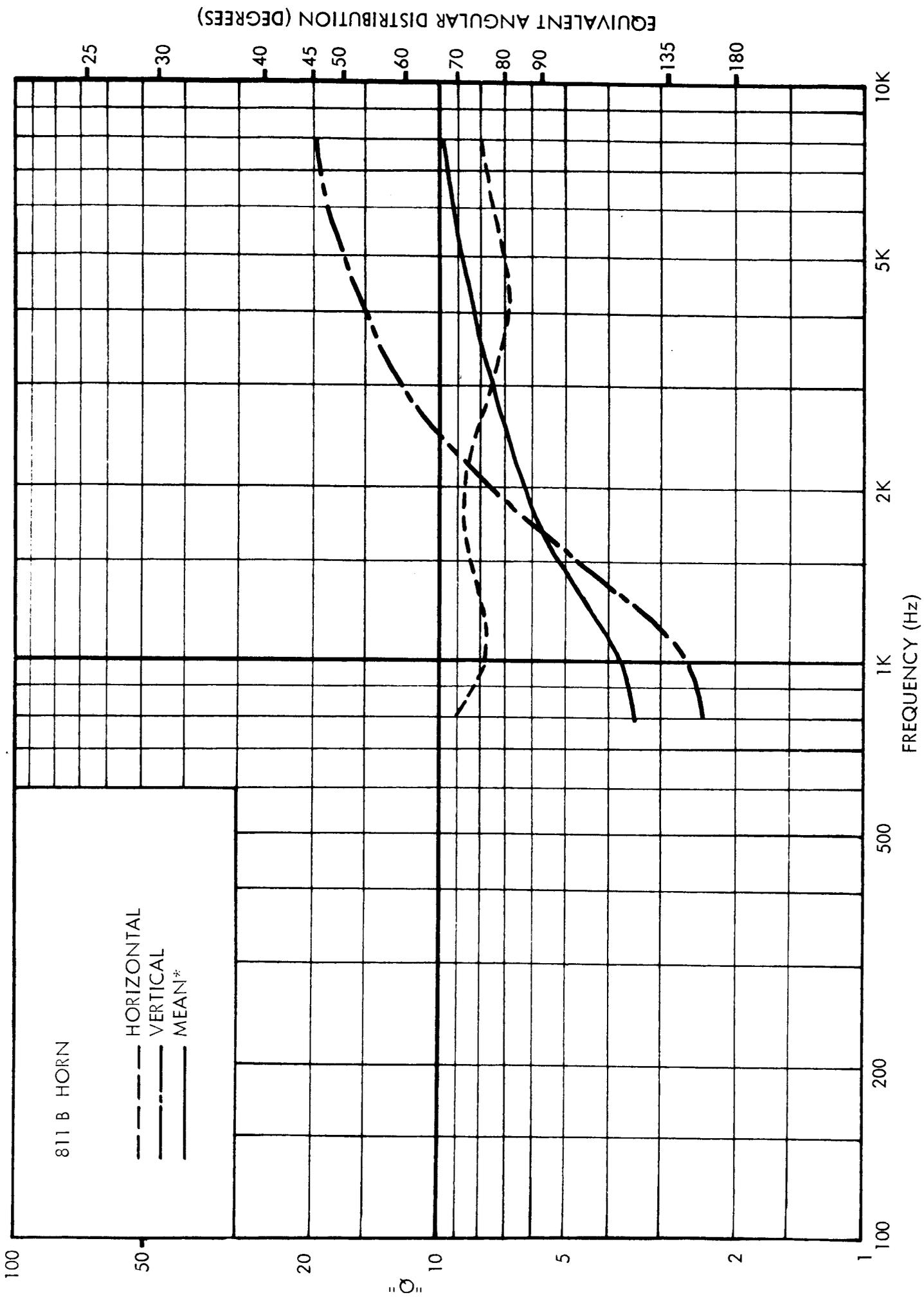
- HORIZONTAL
- .- VERTICAL
- MEAN\*

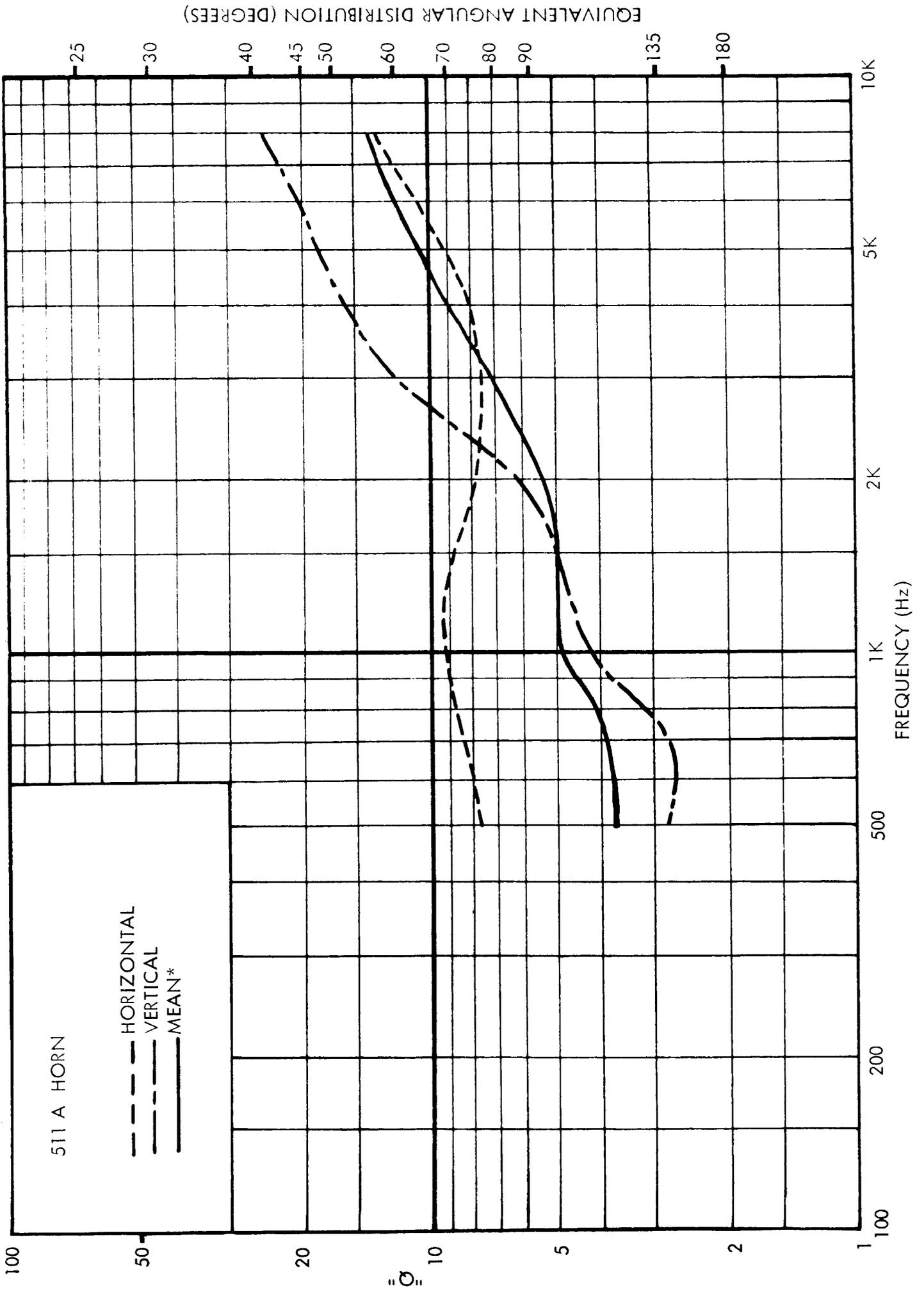
FREQUENCY (Hz)

Q

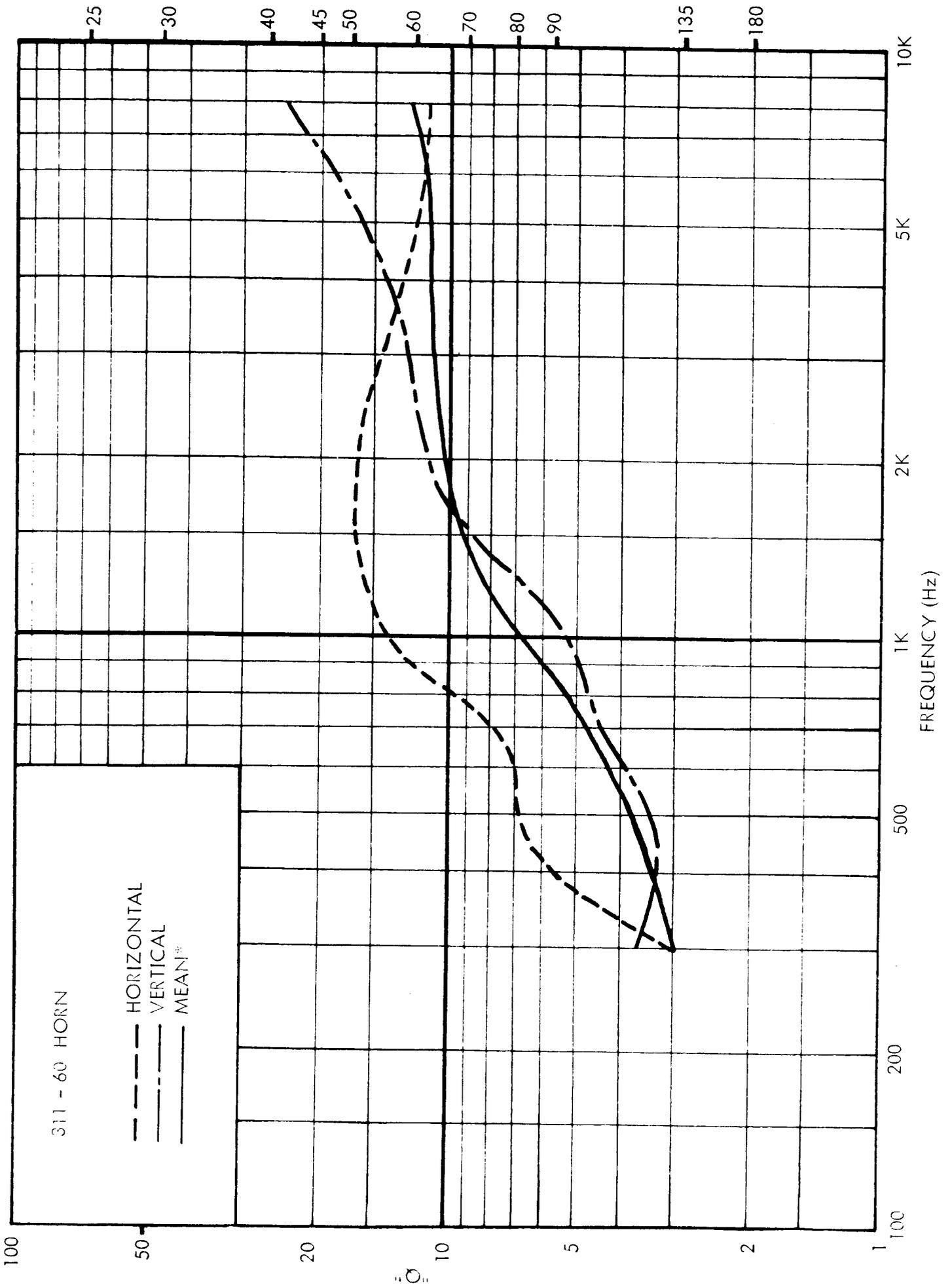
EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

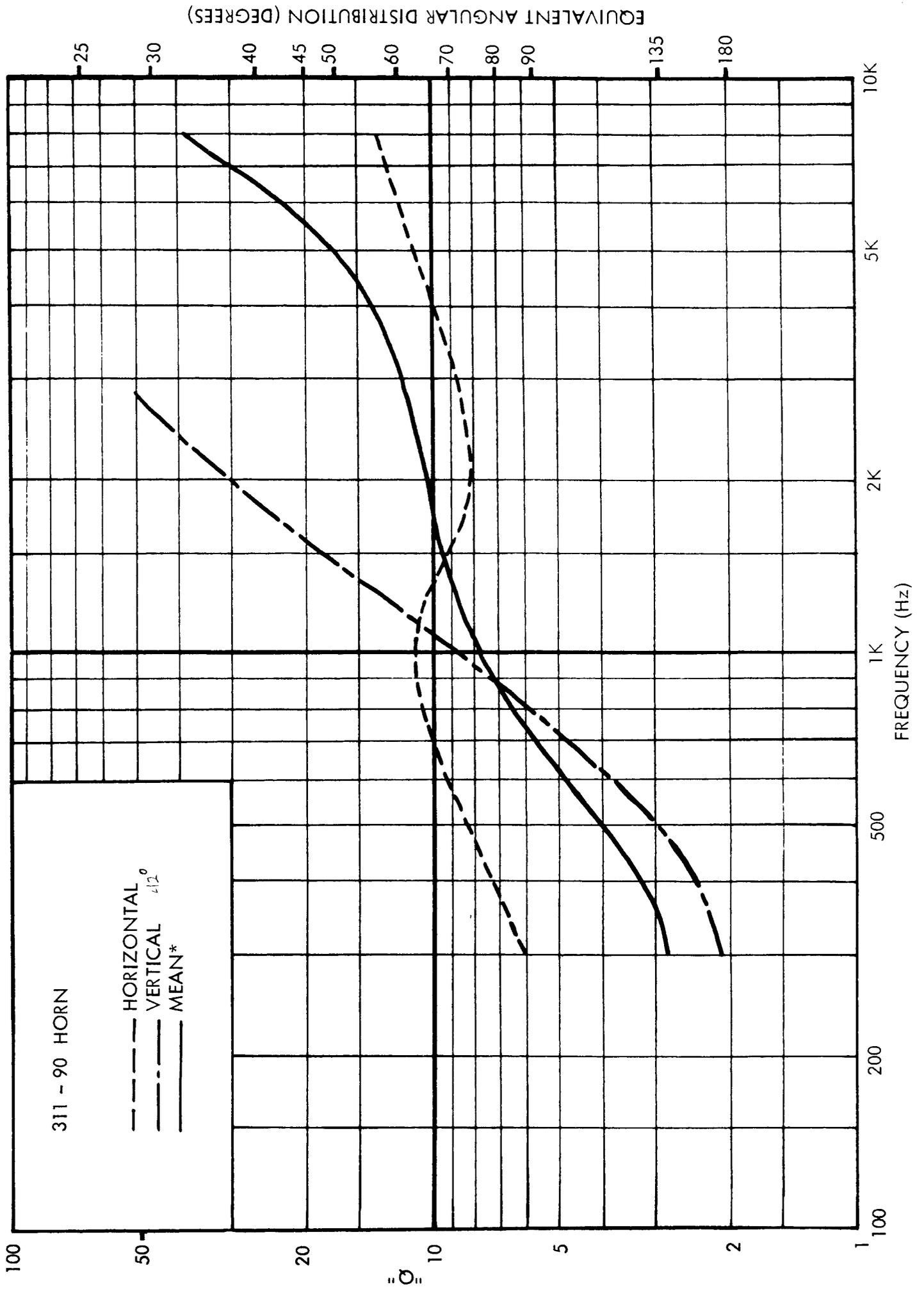




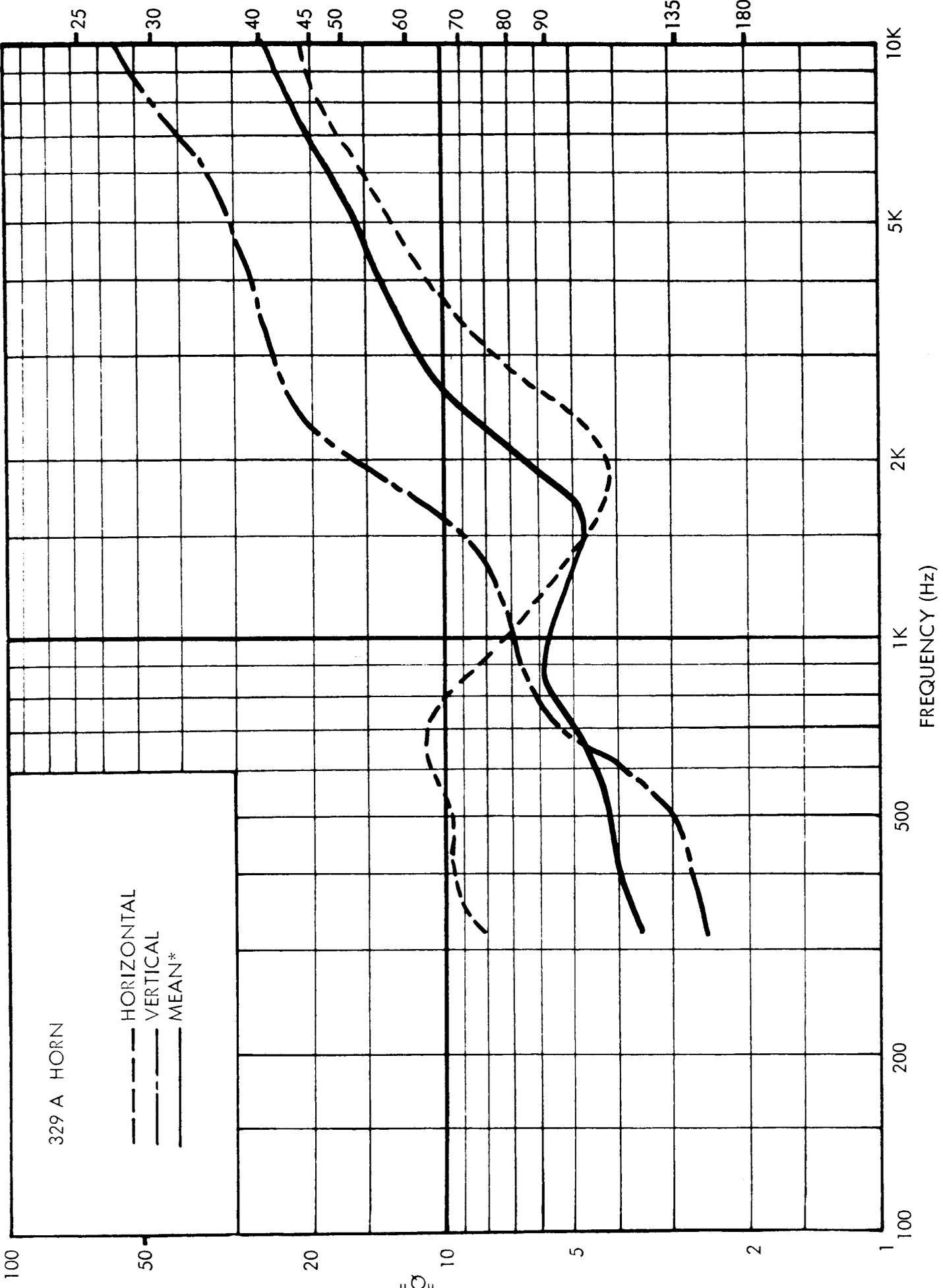


EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)





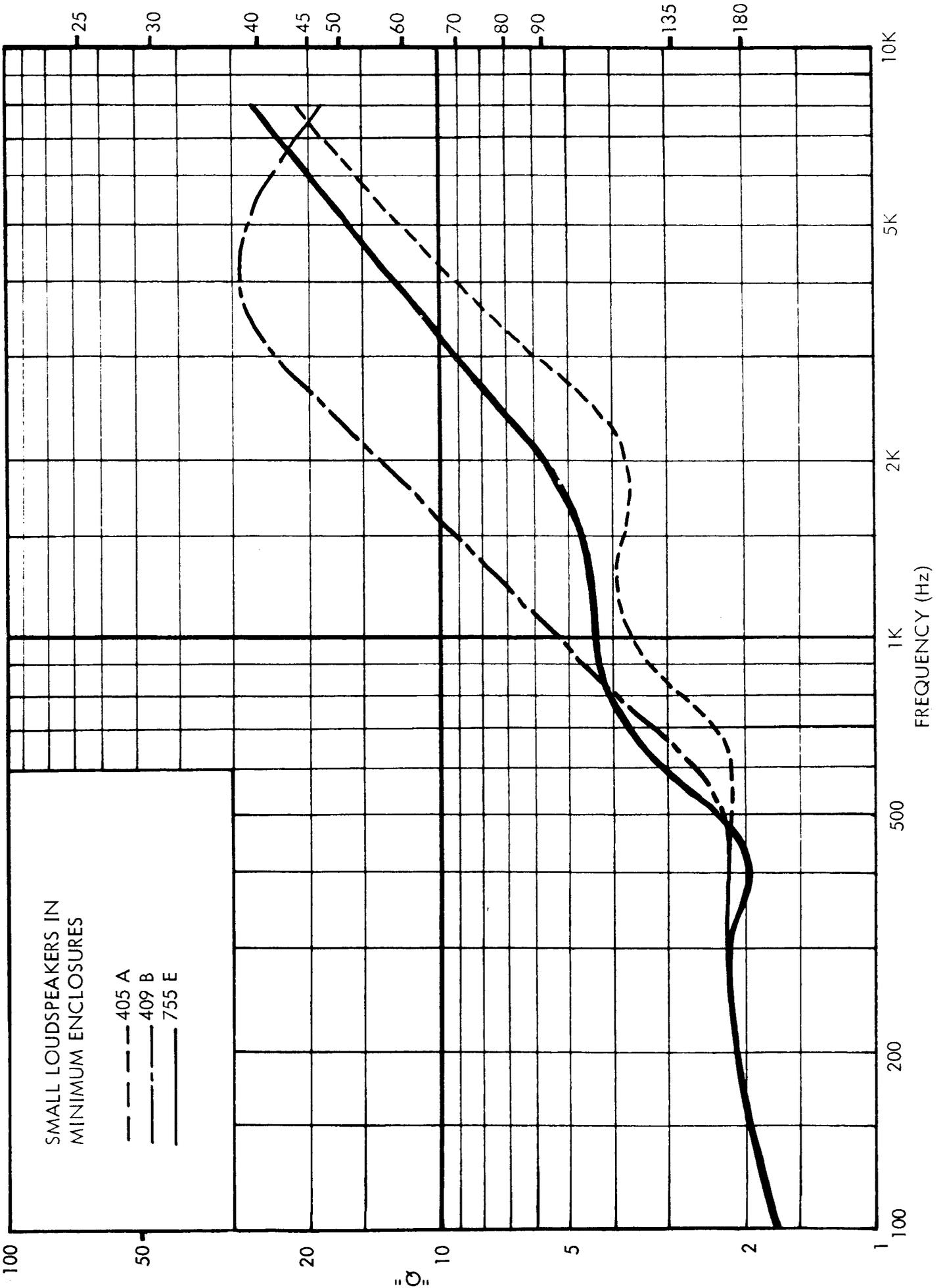
EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

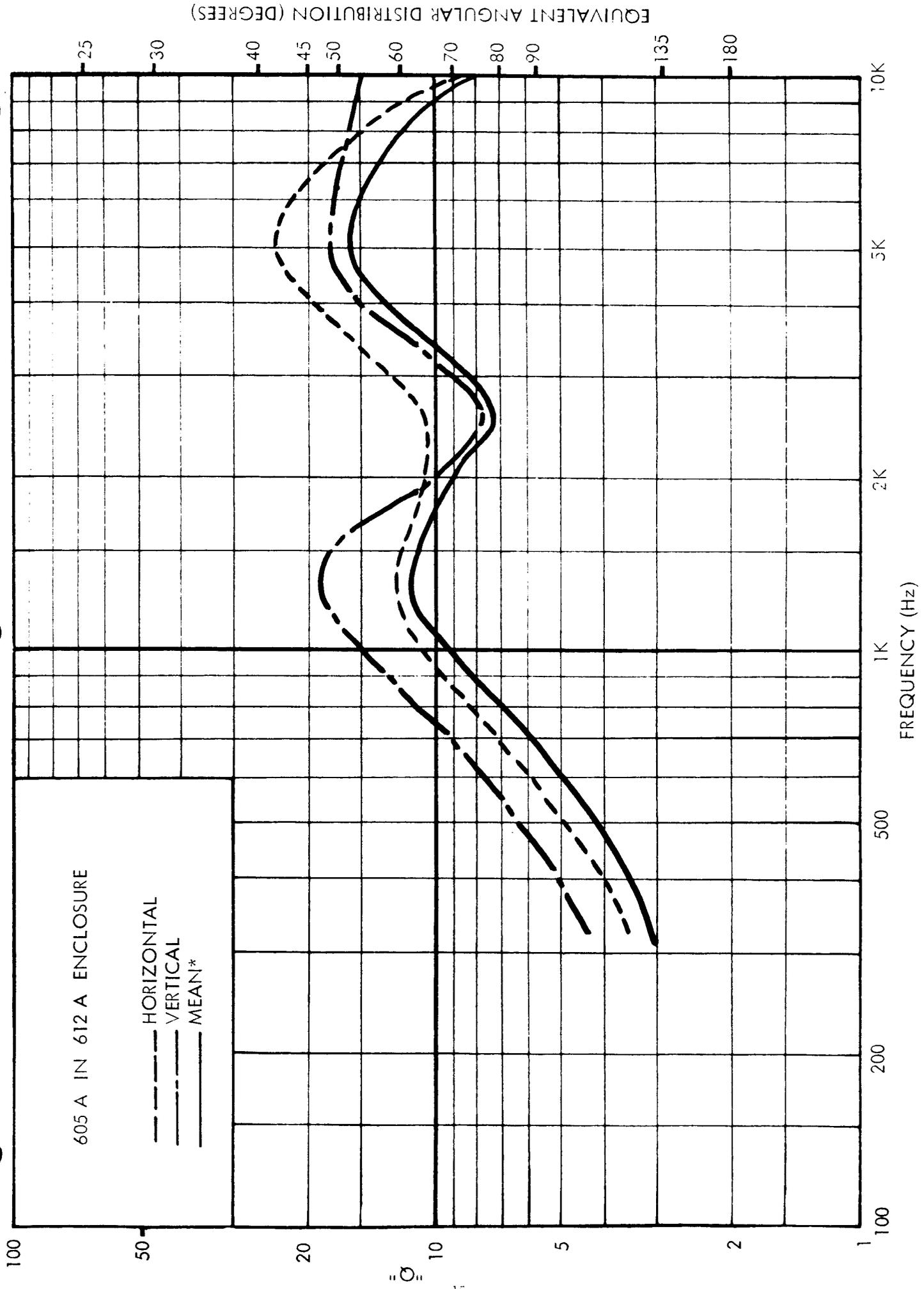


329 A HORN

- HORIZONTAL
- VERTICAL
- · - MEAN\*

EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)



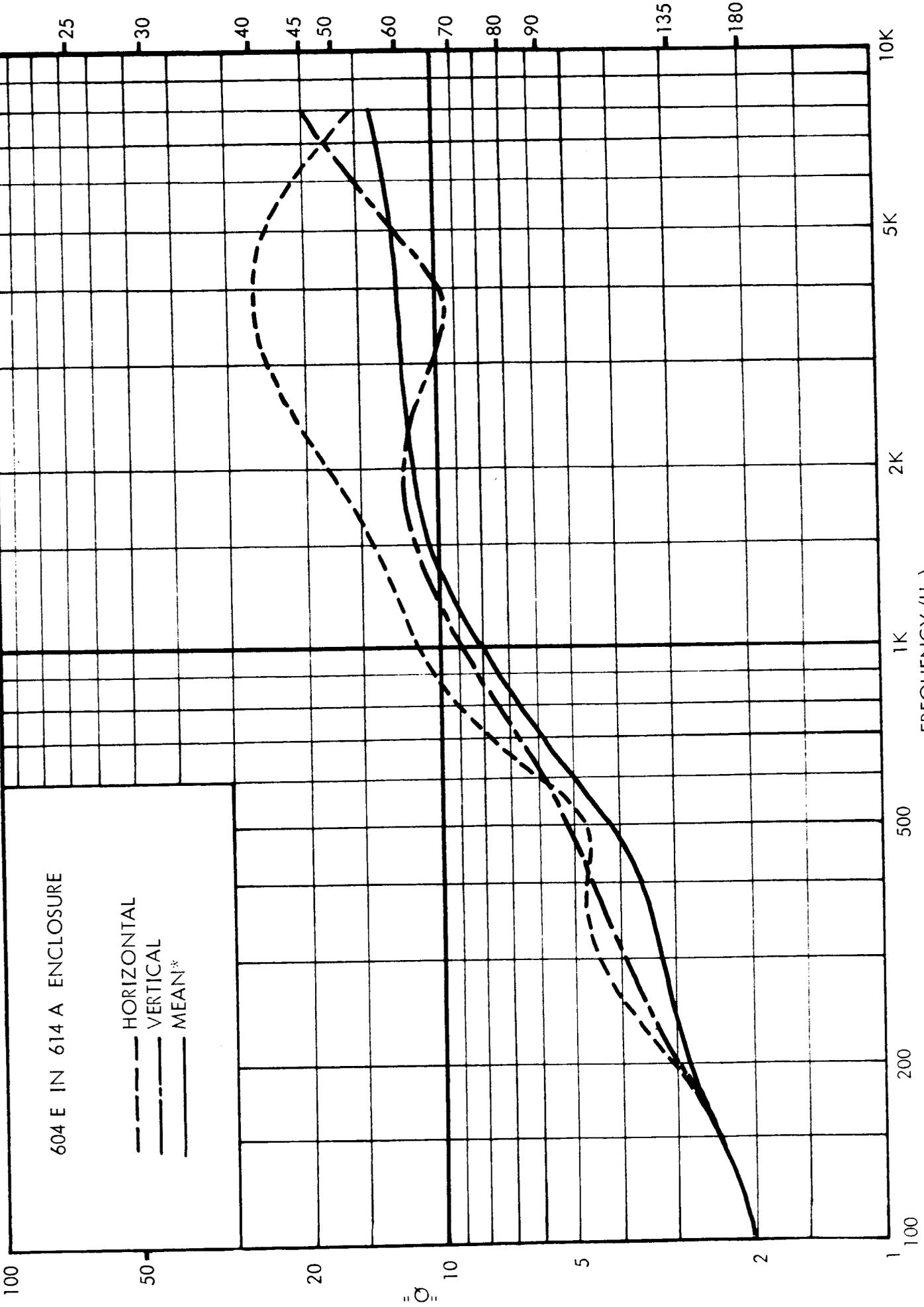


EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

FREQUENCY (Hz)

604 E IN 614 A ENCLOSURE

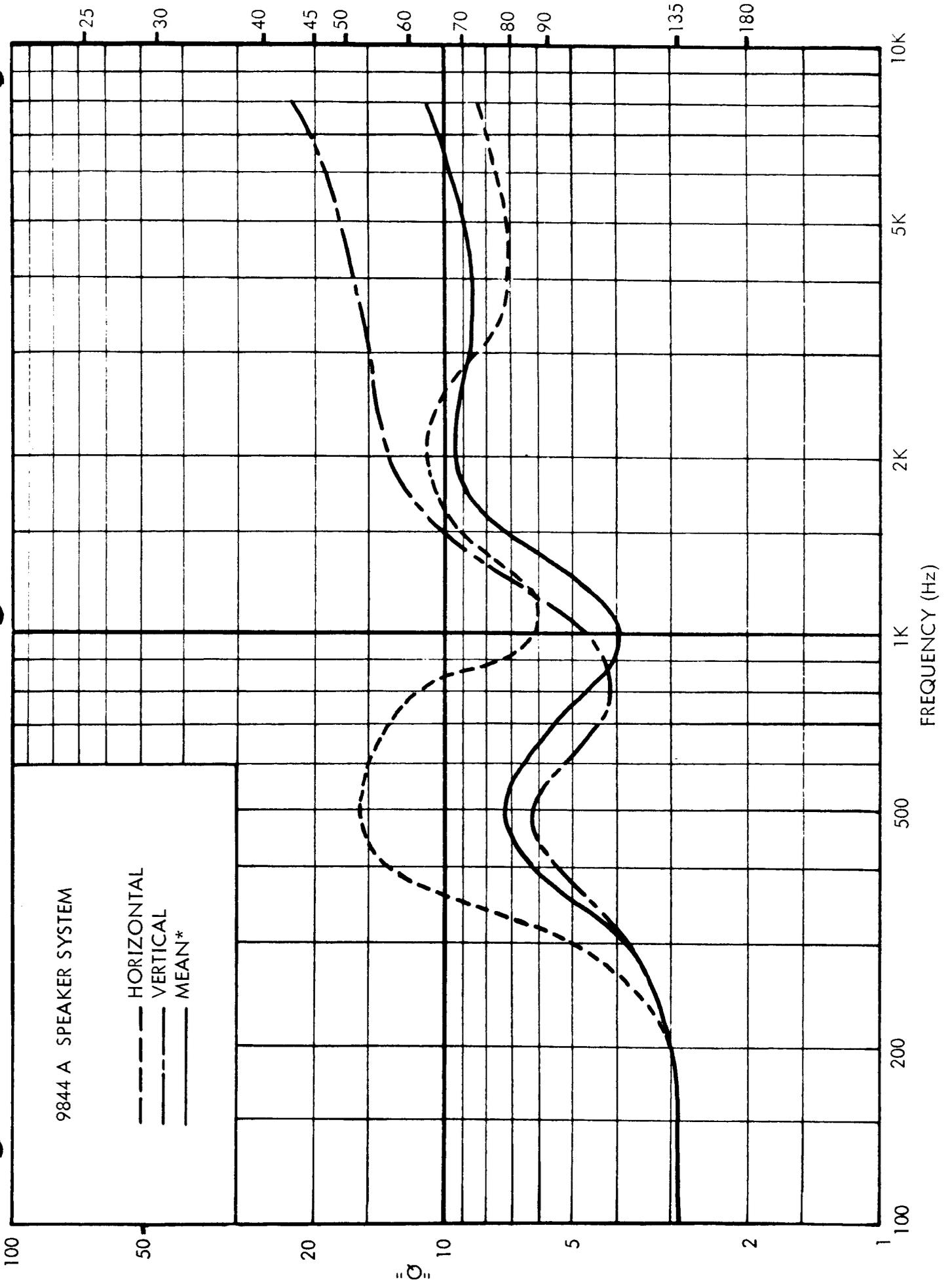
- HORIZONTAL
- VERTICAL
- - - MEAN\*



EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

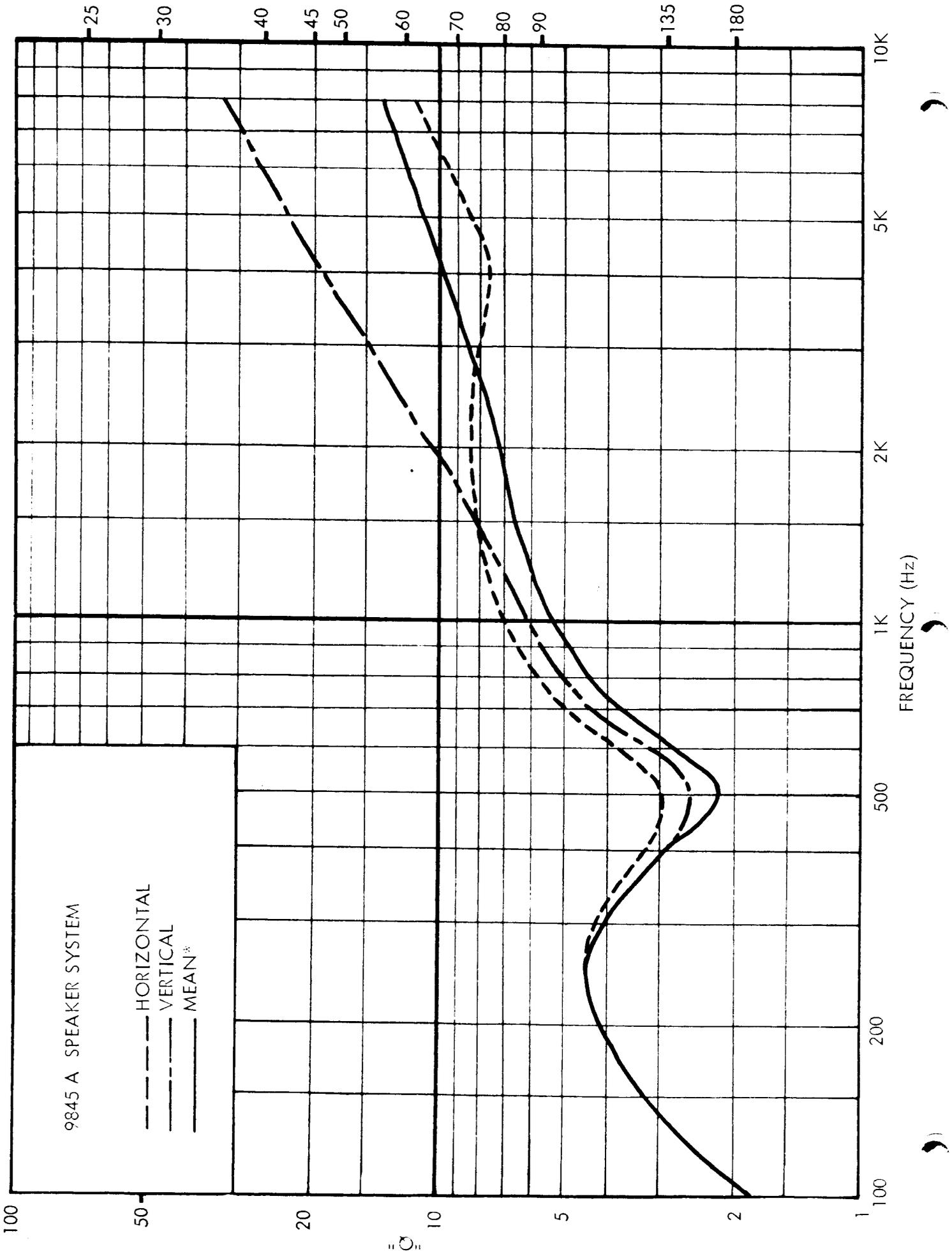
FREQUENCY (Hz)

EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

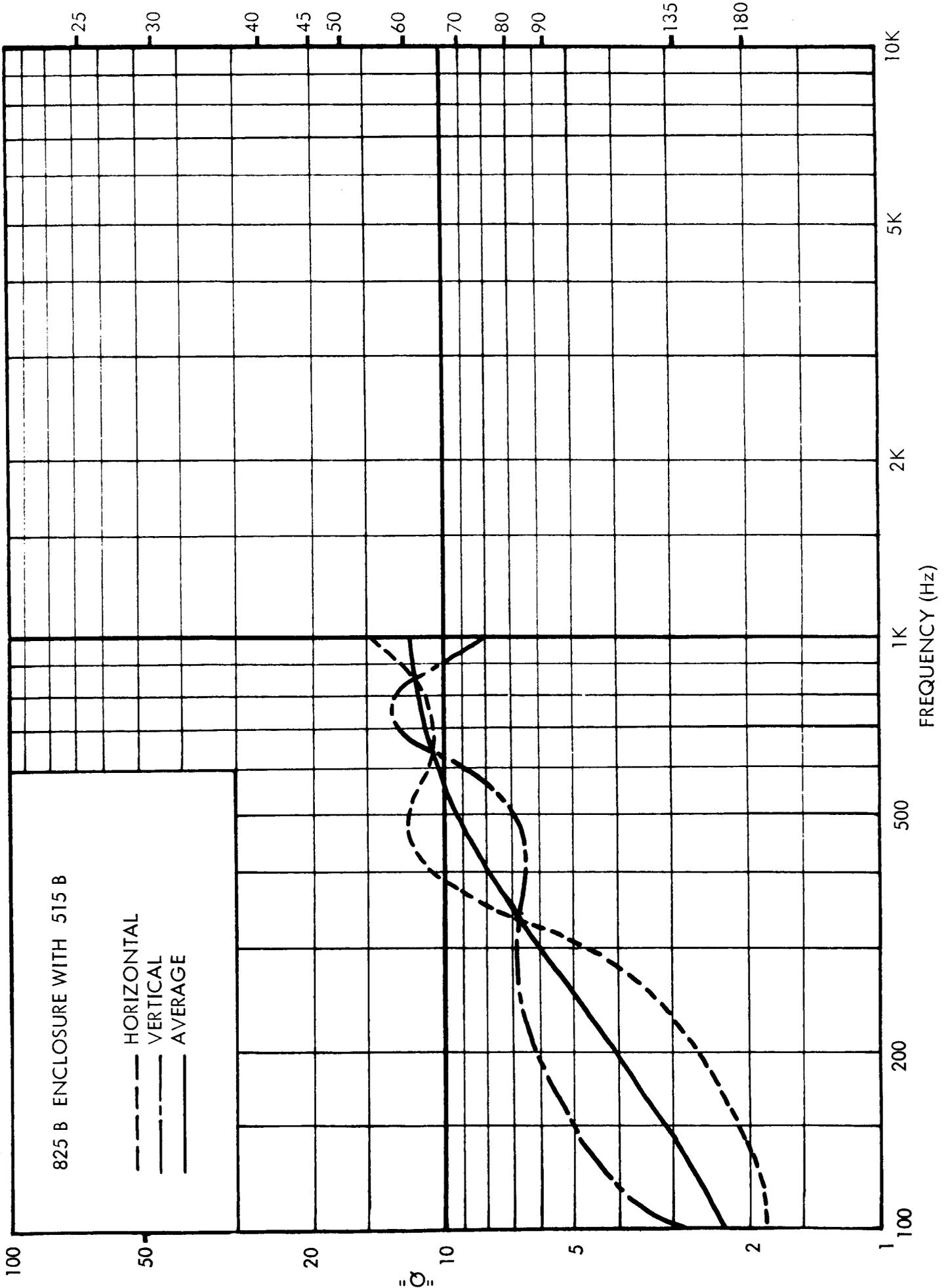


9844 A SPEAKER SYSTEM

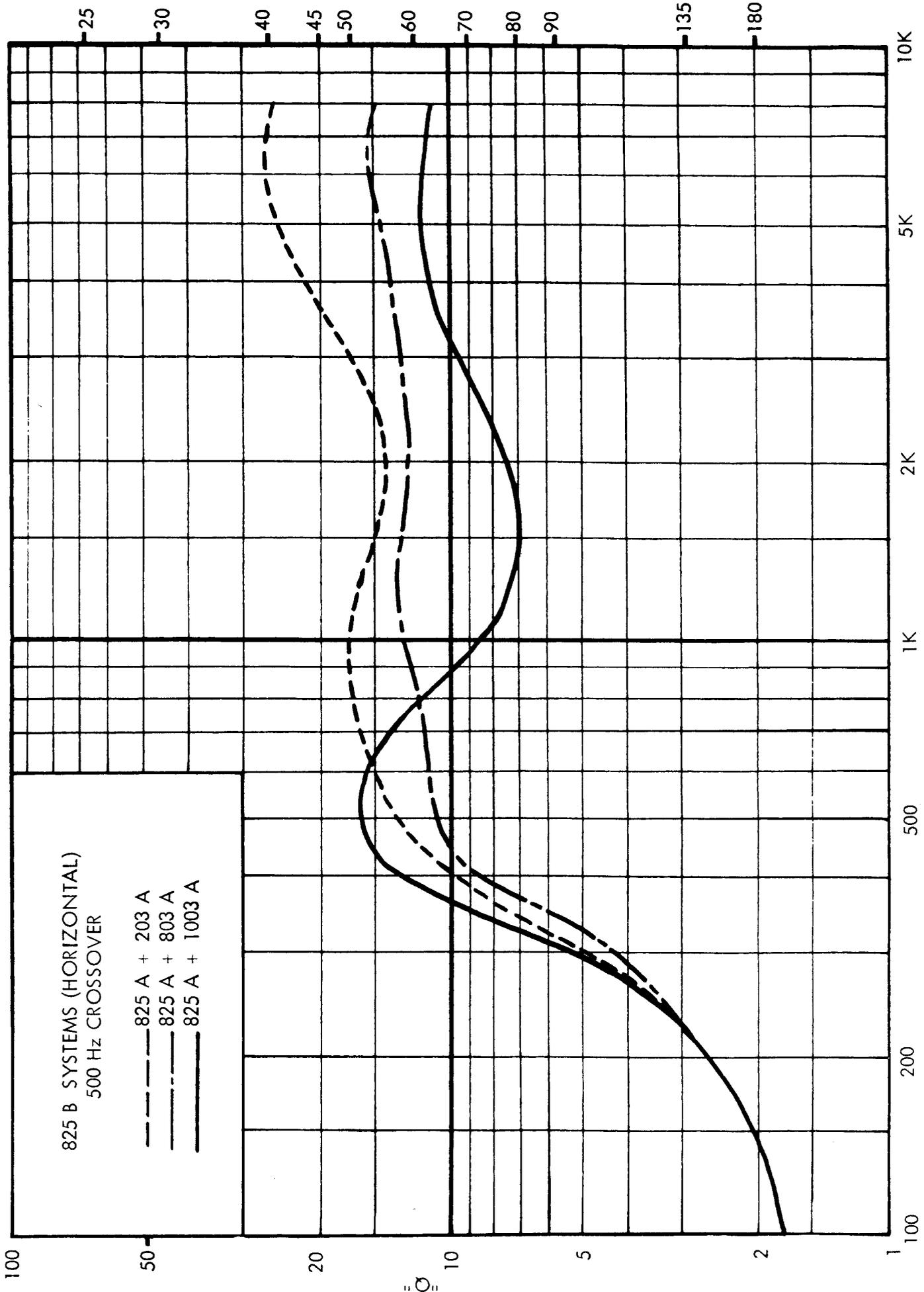
- HORIZONTAL
- - - VERTICAL
- · - MEAN\*



EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)



EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

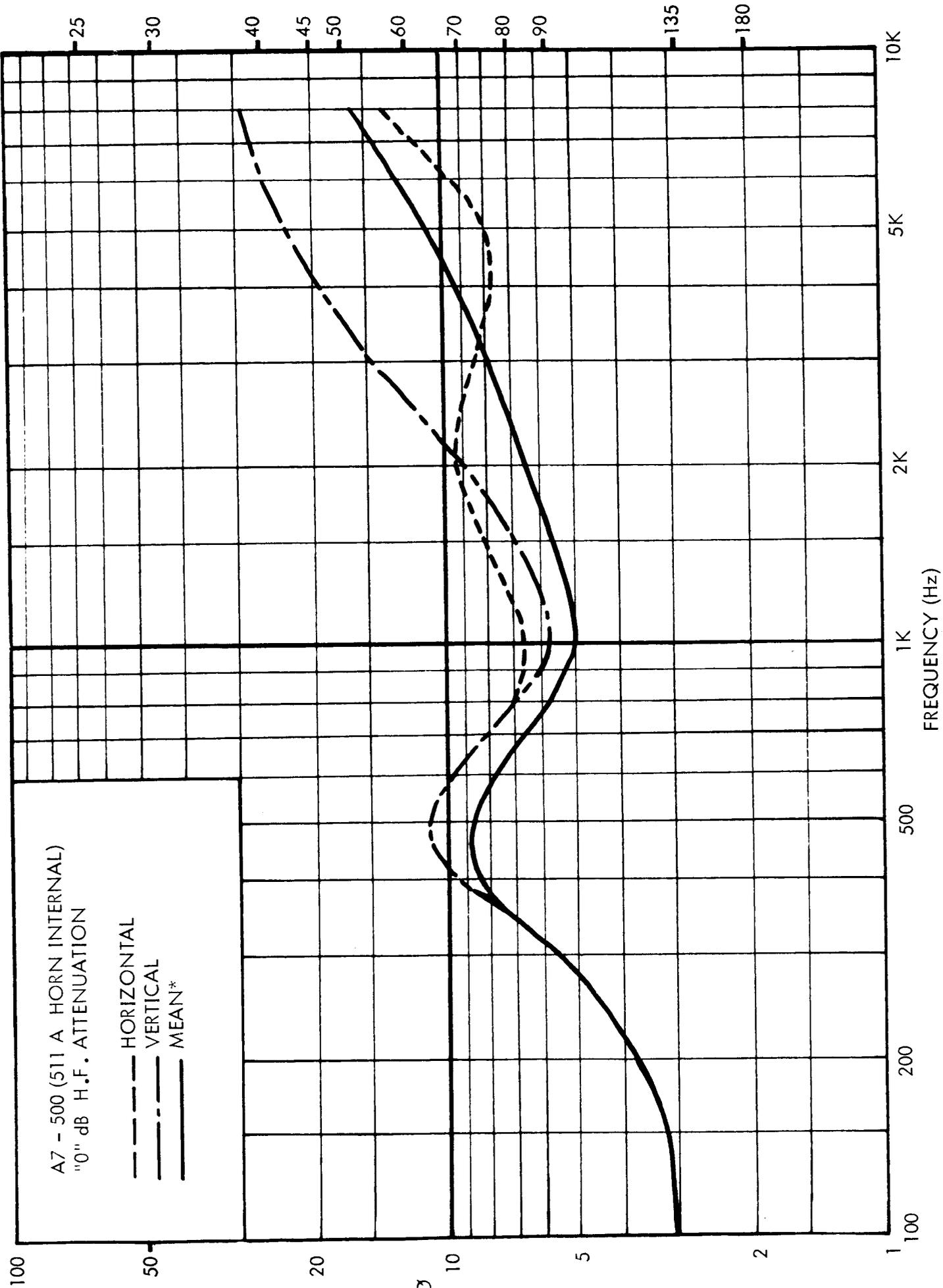


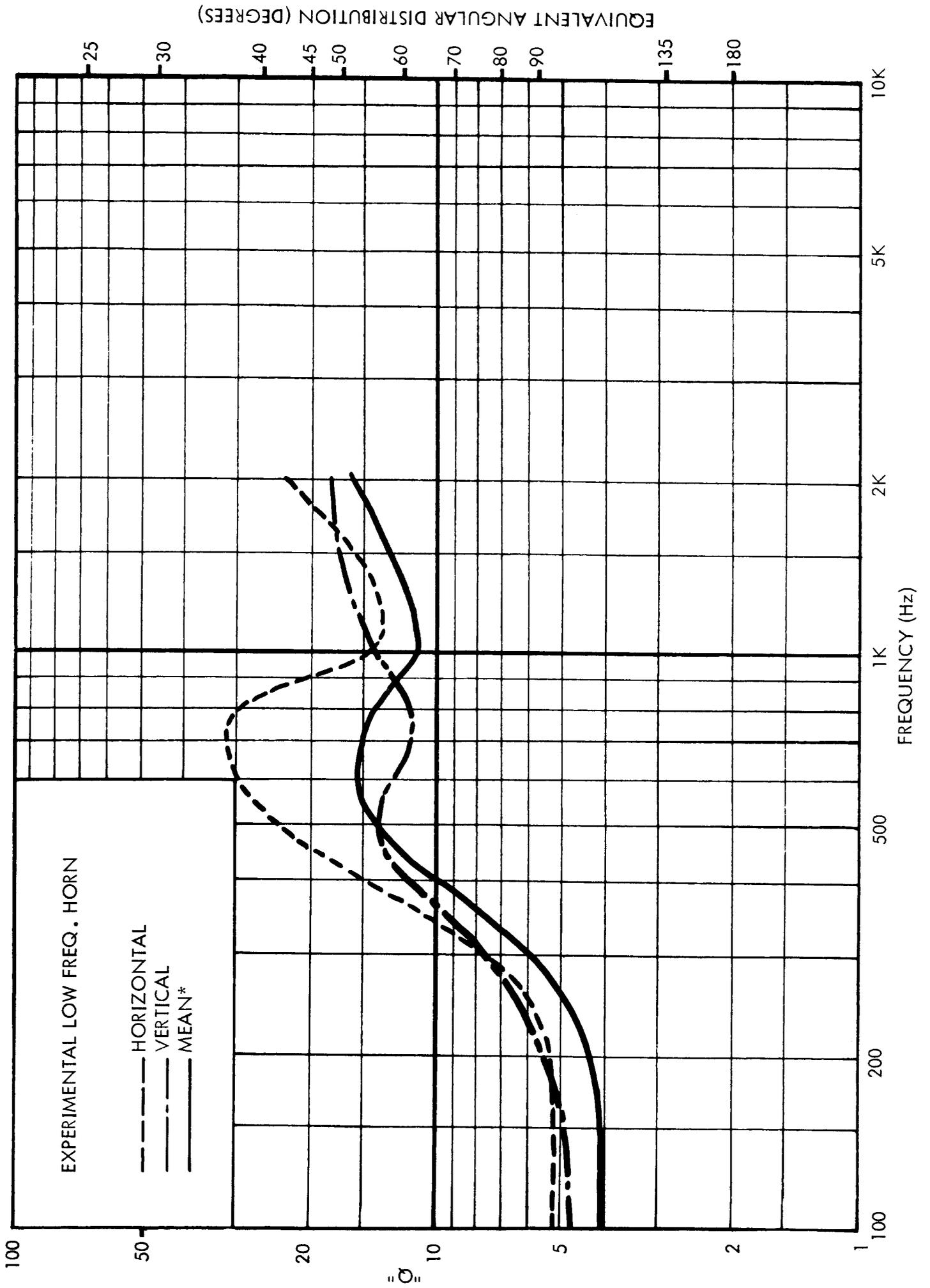
825 B SYSTEMS (HORIZONTAL)  
500 Hz CROSSOVER

- 825 A + 203 A
- · - 825 A + 803 A
- 825 A + 1003 A

FREQUENCY (Hz)

EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)





EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

FREQUENCY (Hz)

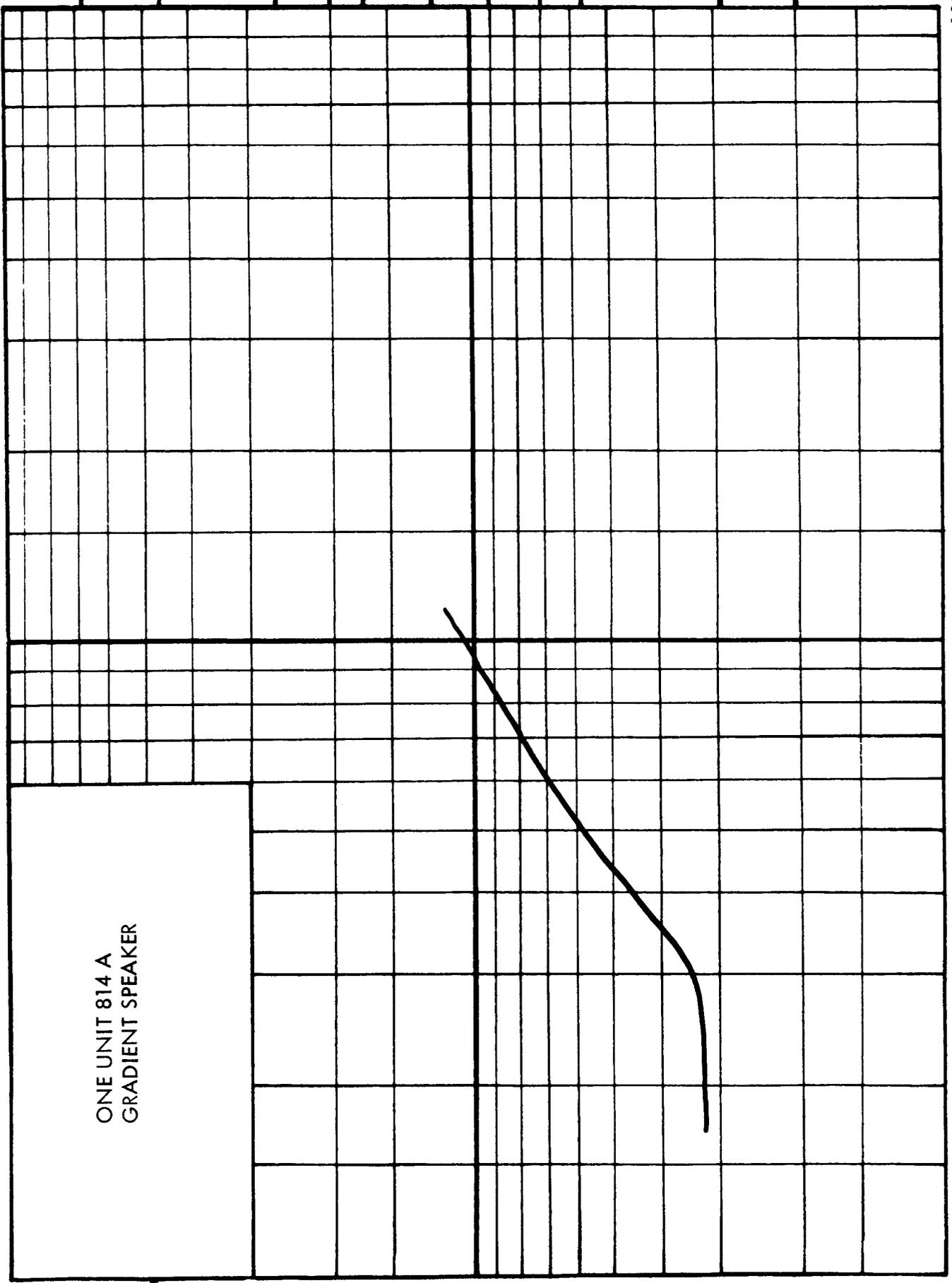
EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

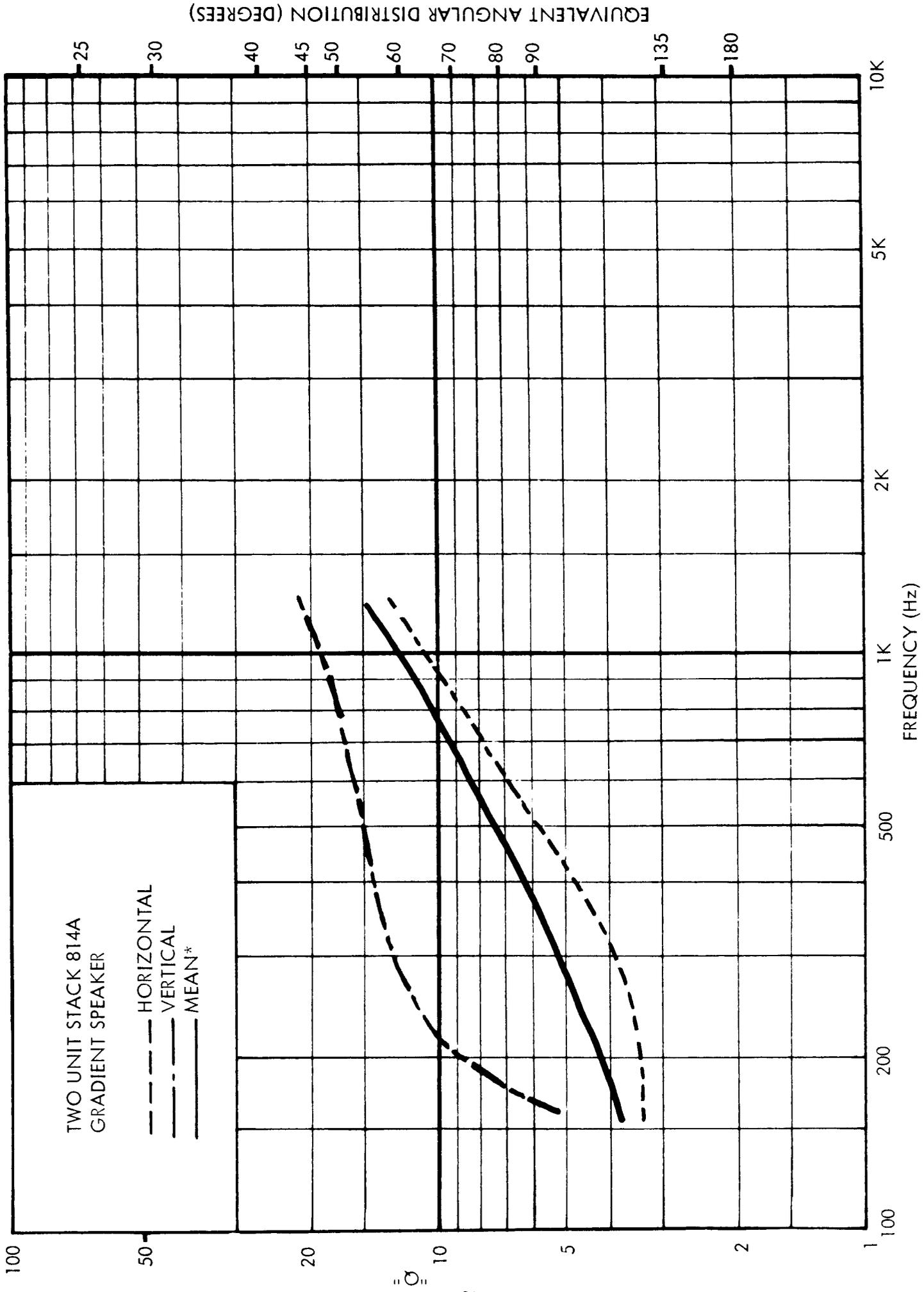
25 30 40 45 50 60 70 80 90 135 180

10K 5K 2K 1K 500 200 100

FREQUENCY (Hz)

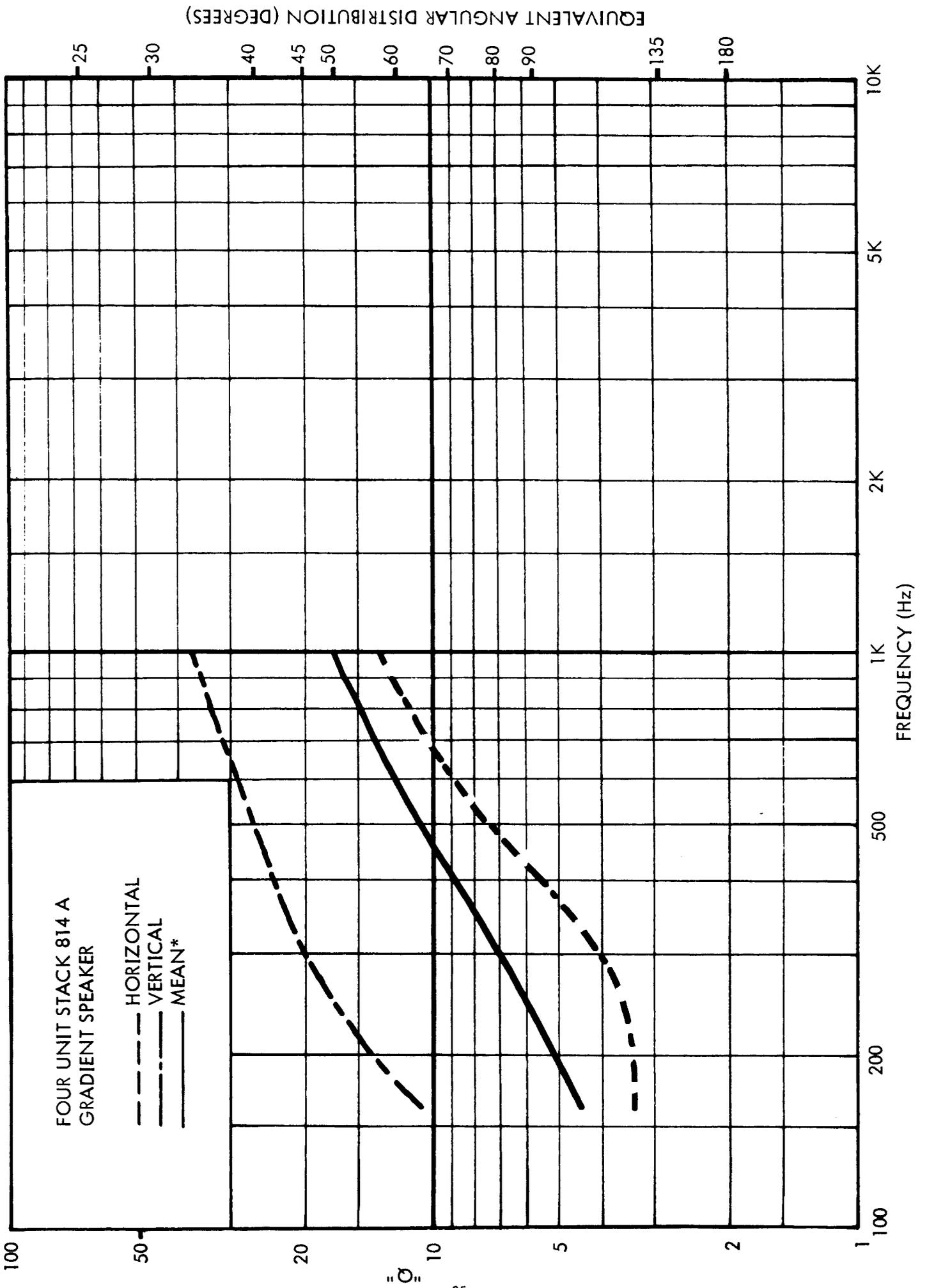
ONE UNIT 814 A  
GRADIENT SPEAKER





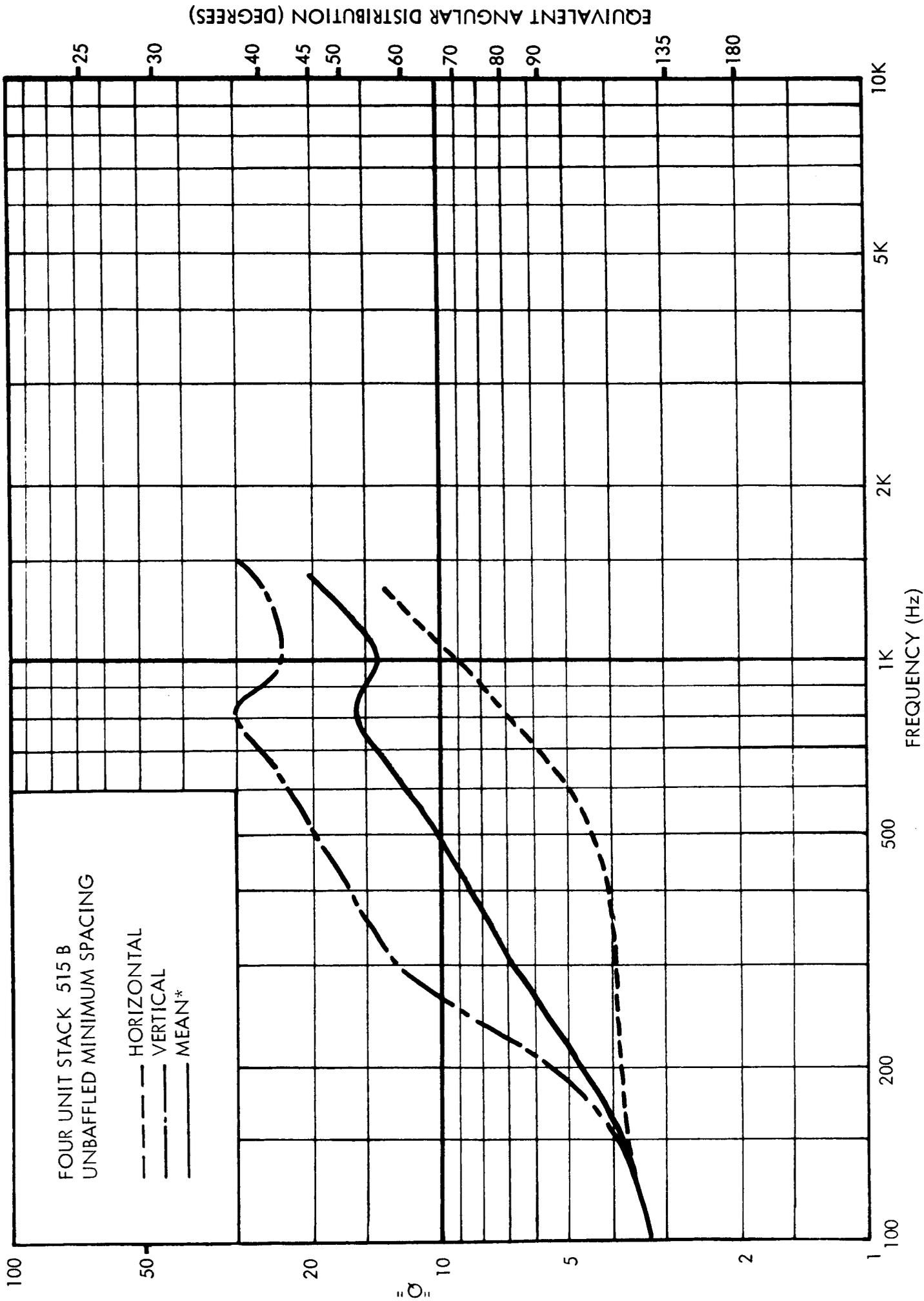
EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

FREQUENCY (Hz)



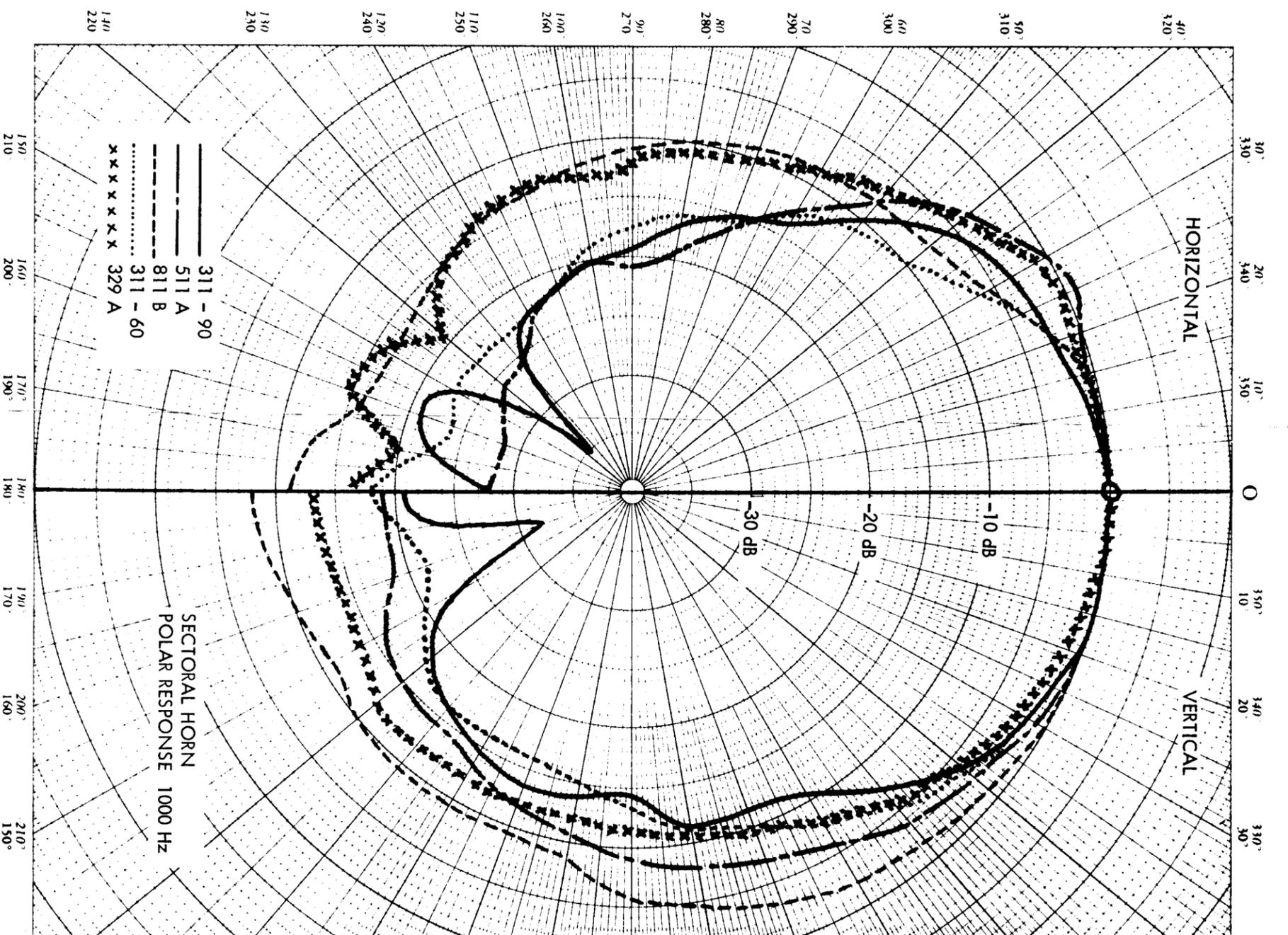
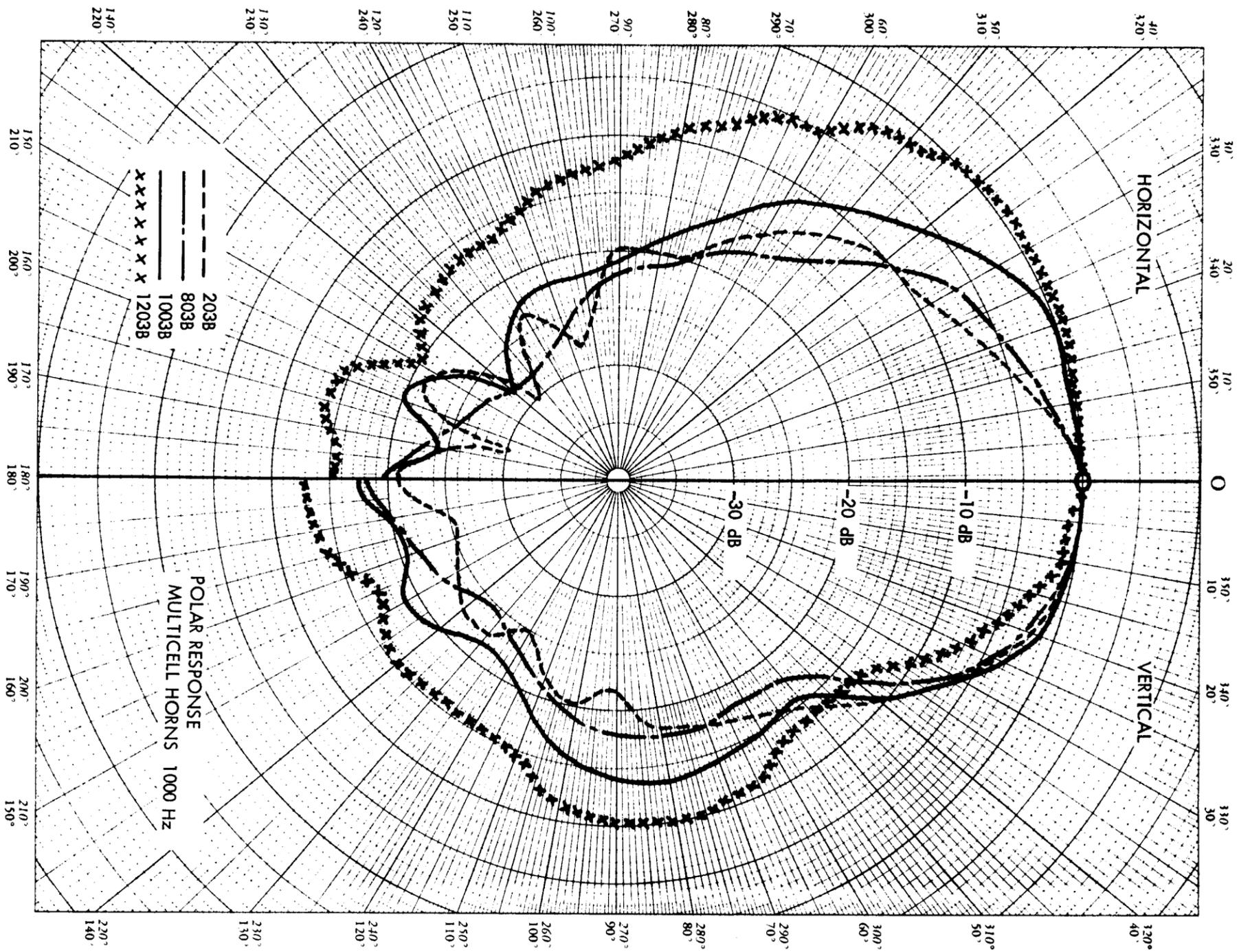
EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

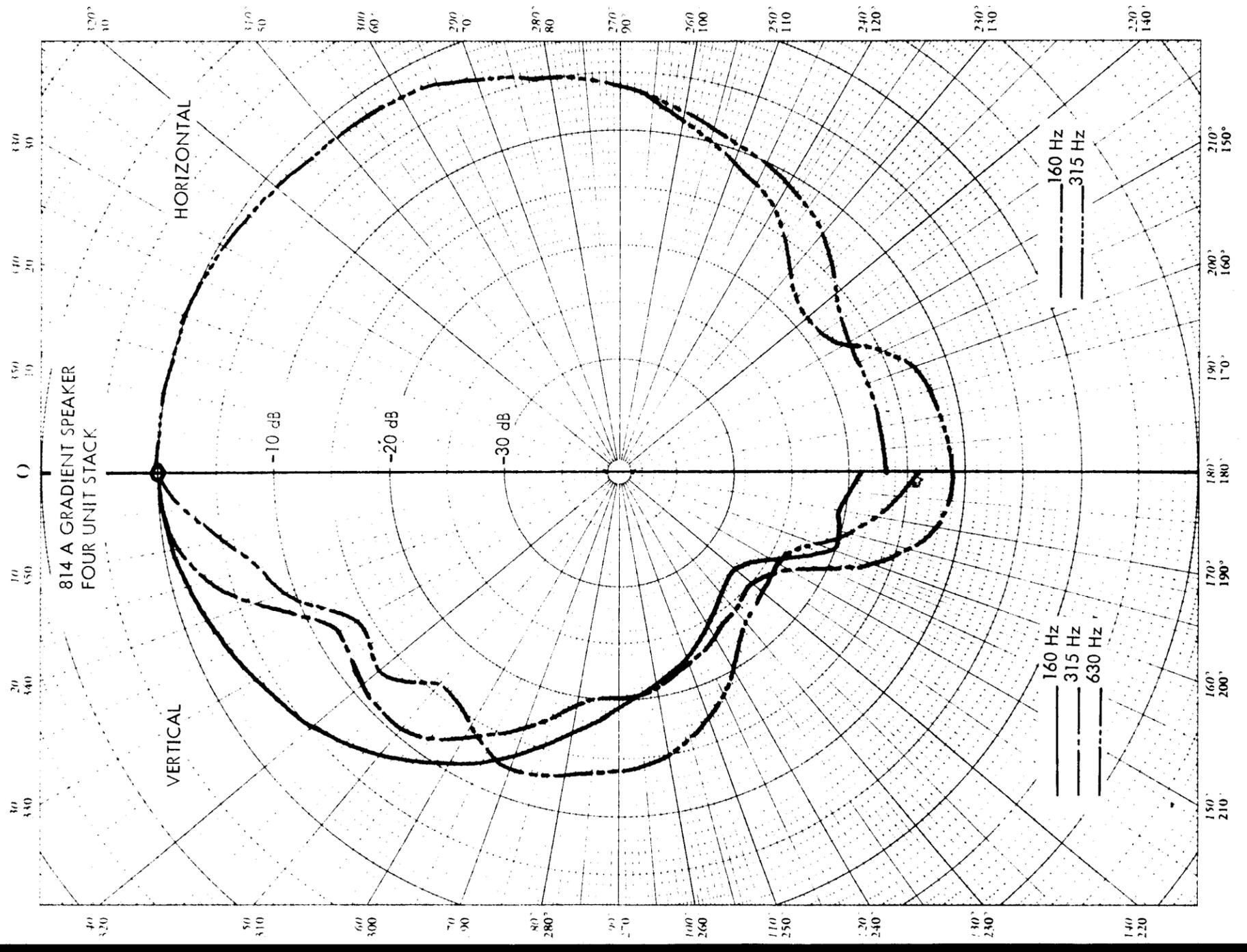
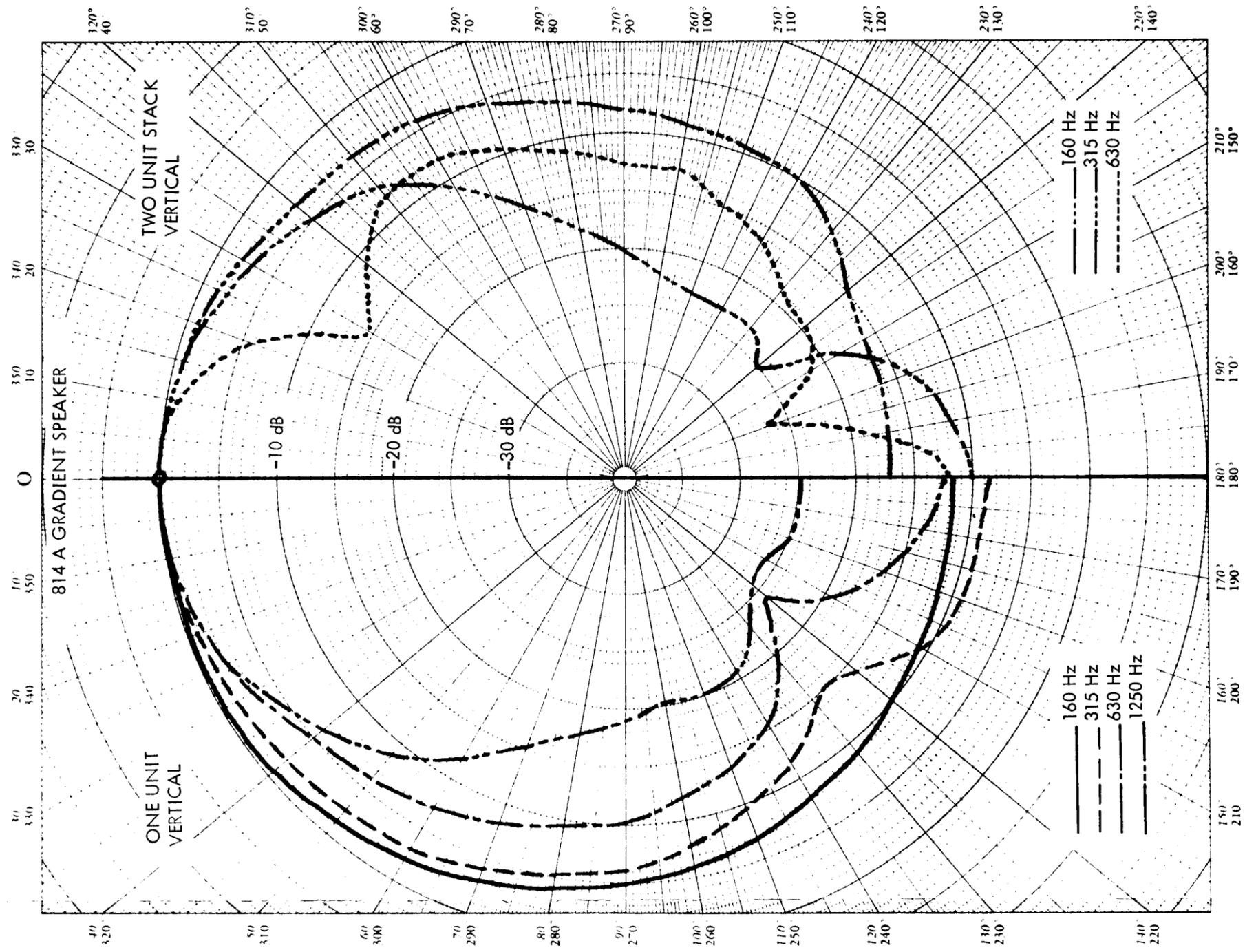
FREQUENCY (Hz)



EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

FREQUENCY (Hz)





EQUIVALENT ANGULAR DISTRIBUTION (DEGREES)

